Tampere University of Technology Electrical Energy Engineering

Tuomas Messo

Use of own programmable calculator is allowed.

## Problem 1 (max 5 points)

Figure 1 shows the control scheme of a grid-connected converter. Answer the following questions:

- a) In which reference frame is the current control implemented in? What is the benefit of using this reference frame?
- b) Justify why the DC voltage can be regulated by changing the value of inductor current d-component.
- c) How would you modify the control system if you implemented the current control in the stationary reference frame?
- d) Why is the term  $\omega_{PLL}$  multiplied with the inductance value and subsequently multiplied with current value and then added in the output of the PI-controller? How does this additional signal loop affect the converter operation during transients?
- e) To which voltage does the converter synchronize its output currents into? How can you see this from the control diagram?

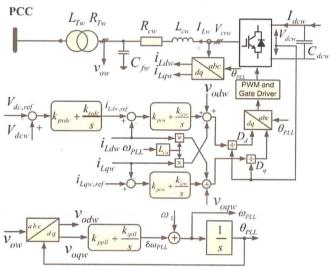


Figure 1: Control system of a grid-connected converter.

## Problem 2 (max 5 points)

A voltage-fed inverter is as shown in Figure 2. Define the average model in the dq-domain. Use the average model to derive the decoupling gains in current control and the grid-voltage feedforward gains. I.e., how should you modify control inputs to decouple current d and q-components and to reduce the effect of grid voltage harmonics? Give the appropriate gains. Note that variables  $c_{\rm d}$  and  $c_{\rm q}$  are now the control variables. (Hint:

Derive the model first assuming  $d_a$  and  $d_a$  as inputs, and subsequently add the effect of gains  $k_1$  and  $k_2$ ).

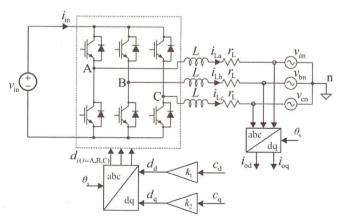


Figure 2: Voltage-fed inverter.

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## Problem 3 (max 5 points)

Transfer function matrix of a grid-connected photovoltaic inverter is given at open-loop in (1).

- a) Draw the control block diagrams that represent the inverter output dynamics in dq-domain and include the output current controllers, sensing gains and PWM modulator gain.
- b) Draw a control block diagram where cascaded control scheme is implemented to regulate the PV voltage. You can assume that DC-side dynamics depend mainly on d-components and that cross-couplings between d and q-components can be neglected.
- c) Use the control block diagram to solve the transfer function of the DC voltage control loop gain.
- d) Explain the tuning process of the cascaded control loops.
- e) Solve the output admittance q-component from the block diagram. You can assume the output current q-component is not affected by any of the d-components.

$$\begin{bmatrix} \hat{v}_{\text{PV}} \\ \hat{l}_{\text{od}} \\ \hat{l}_{\text{oq}} \end{bmatrix} = \begin{bmatrix} G_{11}^{\text{OL}} & G_{12}^{\text{OL}} & G_{13}^{\text{OL}} & G_{14}^{\text{OL}} & G_{15}^{\text{OL}} \\ G_{21}^{\text{OL}} & G_{22}^{\text{OL}} & G_{23}^{\text{OL}} & G_{24}^{\text{OL}} & G_{25}^{\text{OL}} \\ G_{31}^{\text{OL}} & G_{32}^{\text{OL}} & G_{33}^{\text{OL}} & G_{34}^{\text{OL}} & G_{35}^{\text{OL}} \end{bmatrix} \begin{bmatrix} \hat{l}_{\text{PV}} \\ \hat{v}_{\text{od}} \\ \hat{v}_{\text{oq}} \\ \hat{d}_{\text{d}} \\ \hat{d}_{\text{q}} \end{bmatrix}$$
(1)

## Problem 4 (max 5 points)

Three-phase LCL-filter is shown in Figure 3. Solve the average state-space model of the filter in the dq-domain. You can assume that the three-phase input and output voltages are balanced. The zero component can be neglected. Draw the electrical circuits of the filter in dq-domain (separately for d and q-components),

$$\left(\mathbf{x}^{\alpha\beta} = \mathbf{x}^{\mathrm{dq}} \cdot e^{\mathrm{j}\omega_{\mathrm{s}}t}\right), \left(\mathbf{T}^{\mathrm{abc} \rightarrow \alpha\beta} \cdot \begin{bmatrix}k & k & k\end{bmatrix}^{\mathrm{T}} = \begin{bmatrix}0 & 0 & k\end{bmatrix}^{\mathrm{T}}\right).$$

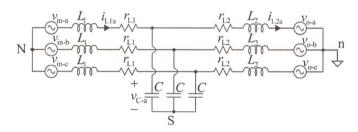


Figure 3: Three-phase LCL-type filter.

$$\begin{split} &\frac{\mathrm{d}}{\mathrm{d}t} i_{\mathrm{L1}}^{\mathrm{dq}} = f\left(v_{\mathrm{NS}}, v_{\mathrm{in\text{-}d}}, v_{\mathrm{in\text{-}q}}, v_{\mathrm{C\text{-}d}}, v_{\mathrm{C\text{-}q}}\right)?\\ &\frac{\mathrm{d}}{\mathrm{d}t} v_{\mathrm{C}}^{\mathrm{dq}} = f\left(i_{\mathrm{L1d}}, i_{\mathrm{L1q}}, i_{\mathrm{L2d}}, i_{\mathrm{L2q}}\right)?\\ &\frac{\mathrm{d}}{\mathrm{d}t} i_{\mathrm{L2}}^{\mathrm{dq}} = f\left(v_{\mathrm{nS}}, v_{\mathrm{C\text{-}d}}, v_{\mathrm{C\text{-}q}}, v_{\mathrm{o\text{-}d}}, v_{\mathrm{o\text{-}q}}\right)? \end{split}$$